# Titanium Standards for Hydrogen Content

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This paper describes the preparation, analysis, and certification of a new series of standard samples. These samples consist of commercially pure titanium containing hydrogen at three levels (32 ppm, 98 ppm, and 215 ppm) and have been designated National Bureau of Standard Standard Samples Nos. 352, 353, and 354, respectively.

#### 1. Introduction

The recent certification of National Bureau of Standards Standard Samples Nos. 352, 353, and 354, for hydrogen content in unalloyed titanium sheet marks the completion of (1) the lengthy process of developing suitable test methods, (2) selecting and producing adequate materials, and (3) the testing necessary for proving homogeneity and certification. The need for these standards resulted from the severe fabrication difficulties which occurred during production of titanium sheet as well as the usual desire to use these standards as reference material for specification compliance.

#### 1.1. Government Titanium Sheet Program

Experiences in aircraft design during and subsequent to World War II indicated a need for materials for aeronautic developments that had a higher strength-weight ratio and better elevated temperature performance than that of the best aluminum or magnesium alloys. Since titanium and its alloys seemed to have these requirements, the Government sponsored extensive programs for the production of titanium sponge and for the fabrication of unalloyed and alloyed sheet.

Although the sponge production program progressed without too many difficulities, the sheet materials produced were so hard and brittle that they could not be fabricated into useful shapes. As a consequence, concerted efforts were exerted to identify and remedy the source of difficulty. Therefore, it was necessary to develop new analytical procedures and techniques for determining the amounts of impurities present in the material. The data obtained were then used for correlation purposes between the physical properties and composition. | Heat No. R-11627) prepared by Republic Steel

In essence, the presence of excessive amounts of hydrogen in the sheet was found to be the main offender. This early research indicated that vacuum annealing could be used as a remedial measure; however, the ultimate answer must lie in the development of metal-processing techniques, as shown by the analytical methods, which would prevent the metal and its alloys from initially accumulating hydrogen in deleterious amounts.

#### 1.2. Analytical Committee

In order to implement the analytical approach, a task group on gas analysis with Dr. T. D. McKinley, Chairman, was organized under the Metallurgical Advisory Committee on Titanium, Panel on Methods of Analysis with Mr. S. Vigo, Chairman. In brief, the efforts of this group resulted in the recommendations for analytical procedures which had been proven by a number of "round-robin tests" and by statistical analyses of the test results. These recommendations, in turn, created the need of reference standards for the hydrogen content of titanium and its alloy products. The Chemical Metallurgy Section was requested to prepare NBS Standard samples at three different levels of hydrogen content from sheet material prepared under the supervision of the Analytical Task Group.

## Preparation of Materials

#### 2.1. Fabrication

The titanium sheet used for making these standards was commercially pure titanium (RS-70,

Corporation, [1]<sup>1</sup> South Division, Canton, Ohio under a contract funded and sponsored by Watertown Arsenal. The cost of the material for the samples was absorbed by Republic Steel Corporation, however, the processing (vacuum annealing, hydrogenation, surface grinding, and specimen cutting) was covered by the Watertown Arsenal contract and furnished to the National Bureau of Standards without charge.

One coil 33 in. wide was cold-rolled to 0.055 in. thickness, then mill annealed, descaled, and cut

into twenty-four 96 in.-long sheets.

#### 2,2, Hydrogen Equilibration

The program for this sheet material was directed towards the production of a series of samples at three different levels of hydrogen content in accordance with the following:

Sheet No.	Group	NBS sample No.	Hydrogen elm.	Permissible limits for bydrogen	Permissible   mits for  scient ansl.
1-8 9-16 17-24	T T	352 363 354	1917 int 200 200 200	99™ 26-45 90-110 190-210	% ±10 ±5 ±5

The sheet stock, as produced, contained 85 ppm of hydrogen; thus it was necessary to hydrogenate Groups I and II sheets to bring their hydrogen contents above the desired amounts. This operation consisted of submersion in a bath of sodium hydride, followed by a sulfuric acid wash to clean the sheets. Following the hydride treatment, the sheets were grit blasted in order to create a high surface-to-volume ratio which should enhance the out-gassing and equilibration treatments.

For the hydrogen equilibration treatment, the manufacturer has shown that at 1,300  $\pm 5$  °F (704  $\pm 3$  °C) the equilibration pressures were 1, 8, and 40 $\mu$  for 30, 100, and 200 ppm hydrogen, respec-

tively.

The procedure employed by the producer consisted of clamping each of four sheets at 2-in. intervals within a vertical retort annealing furnace; evacuating prior to heating to prove the furnace airtight and until a leak-rate of < 60  $\mu$ /hr was achieved, then the heat was applied. As the load reached 750 °F (399 °C) the furnace was blanked off to insure against pumping off of any hydrogen. After stabilizing at the 1,300 °F (704 °C) level, oil-diffusion pumps were employed to attain the desired pressures. These conditions were maintained for 12 hr, following which the samples were cooled to room temperature over a period of 72 hr under conditions which maintained uniformity of temperature throughout the sheets to less than 10 °F (6 °C) in order to minimize nonuniform distribution of the hydrogen in the sheets.

The test results on Group III (30 ppm) sheets revealed a high degree of uniformity. These sheets

were nibbled into ¼ in. squares, vapor degreased, dry-tumbled, and shipped to the National Bureau of Standards.

The preliminary test results on Group I and II indicated that a hydrogen content gradient was present in the sheets. In this instance it was decided, therefore, to cut the sheets into 12 to 14 pieces 12 in. × 15 in. and 18 in. × 15 in. Each of these sheets was then tested and only those which had hydrogen contents within the general limits set up for the two groups were processed into ¼ in. squares and forwarded to NBS. The identities of these sheets were maintained by packaging the squares from each 12 in. × 15 in. and 18 in. × 15 in, sheet separately. After each sheet had been tested at NBS it was then possible to narrow the limits of the hydrogen content even further for the final samples, which are the present published limits.

#### 3. Test Method

There are four basic analytical procedures available for the determination of hydrogen content of titanium. These are the vacuum-fusion, hot-extraction, equilibrium-pressure measurement, and oxidation methods.

In order to compare these methods several "round robins" have been conducted by interested groups, among which are Materials Laboratory of Wright Air Development Center [2] an ad hoc group on chemical analysis of the Materials Advisory Board Titanium Alloy Sheet Rolling Panel, and an industrial group working with titanium. It was found that the hot extraction method at 1,400 °C appeared to be the most practical method in the case of hydrogen as a considerable number of specimens can be analyzed in one working day as against four or five for the vacuum-fusion method, and good reproducible results are obtainable.

It was decided, therefore, to use the hot-extraction method at 1,400 °C which is described in the following paragraphs. This method is now in the process of being recommended by the Metallurgical Advisory Committee on Titanium, Panel on Methods of Analysis to the American Society for Testing and Materials for certification as a standard method.

The specimens to be analyzed were selected at random from a particular group, cleaned of any oil, grease, and foreign matter by washing with ethyl ether, weighed, and inserted into the control arms of the vacuum fusion furnace. A quartz crucible was then packed with a new graphite crucible and graphite insulation inserted, and hung within the furnace assembly. The entire apparatus was then closed and vacuum slowly applied until a suitable vacuum (as observed with a McLeod gauge) was obtained with the mechanical pumps and the diffusion pumps. The furnace was slowly heated by induction to a temperature of 2,100 °C, which was maintained for approximately 1 to 1½ hr in order to outgas the graphite crucible and provide for a sufficiently low blank correction which was considered a constant. The temperature was then lowered to an operating temperature of 1,400 °C ±20 °C and the vacuum

<sup>&</sup>lt;sup>1</sup> Figures in brackets indicate the literature references at the end of this paper.

checked to insure that an operating pressure of less than 1 x 10-3 mm Hg was maintained. The blank was then run, utilizing the method and collection times to be used with the specimens. If the blank was sufficiently low it was considered a constant and specimens run immediately. However, it was in the interest of accuracy and good practice that the blank correction be repeated every five or seven specimens in order to insure against any unusual or unexpected changes in values. If the blank correction was excessive, the furnace temperature was raised for another out-gassing until a suitably low blank correction was obtained.

When a suitable blank (approximately  $2 \times 10^{-7}$  g  $H_2$ ) had been obtained, the specimen (being non-magnetic) was moved along the control arm with a magnetic pusher and was introduced into the furnace at 1,400 °C. At this temperature, which was below the melting point of the specimen, only the hydrogen gas was liberated and collected as a total volume of gas in the Toeppler Pump for a period of 20 min. The gas was then transferred by the pump into a previously evacuated McLeod gage where it was measured as the total quantity of hydrogen liberated from the specimen. By using this figure and making suitable corrections for the blank and the calibration of the McLeod gauge, the percentage or parts per million of hydrogen gas in the specimen could be computed and reported.

## 4. Tests and Results

## 4.1. NBS Sample No. 352

The low hydrogen sample, designated Group III originally, now numbered NBS 352, was originally set up to have a hydrogen content in the range 25 to 45 ppm.

Because this material from the different sheets was mixed at the manufacturer's plant, it was not possible to segregate specific batches with respect to position in the original sheets. As a consequence, random samples were selected by a quartering process from the bulk after it had been subjected to through mixing. The test results from this material are given for the individual laboratories in tables 1 to 6, and the combined results by several cooperating laboratories are given in table 7.

### 4.2. NBS Sample No. 353

The intermediate hydrogen sample was prepared in the same manner as the low hydrogen material. However, the test samples were selected from the nibbled specimens from the 12 in. x 15 in. and 18 in. x 15 in. sections which were cut from the original sheets, as previously described.

The results for this selected material are given for the individual laboratories in tables 1 to 6, and the summary of results obtained from the combination of the test data from the various cooperating laboratories is given in table 8.

#### 4.3. NBS Sample No. 354

The high hydrogen material was prepared in the same manner insofar as sampling is concerned as was sample No. 353. The results for the material selected for the standard are given for the individual laboratories in tables 1 to 6, and the results obtained by the combination of the results from the various laboratories is given in table 9.

## Standard Samples

The availability of these three new standards for the hydrogen content of titanium has recently been announced by the National Bureau of Standards. A series of tests recently conducted by one of the leading producers of titanium, made on the material finally selected for the standards, gave excellent correlation with the test results shown in the following tables.

TABLE 1. Battelle Memorial Institute

	Observed values			
!	Sample No. 352	Sample No. 352 Sample No. 253		
	pp:m 30. 8 30. 8 81. 8 30. 6 30. 0 81. 2	99.5 94.5 95.5 99.5 99.5 98.5	9 pm 204 206 211 210 213 217	
Total No. det	6 80.9 6 1.9 1.8 30.0	5 95.4 2.7 2.8 5.8 99.5 92.7	5 209. 0 5. 9 2. 9 16 217 201	

Norm: In tables 1 through 6 the standard deviation and coefficient of variation were computed as follows:

Standard deviation  $= t = \sqrt{\frac{Z(X - \overline{X})^2}{n - 1}}$ where  $\frac{X}{=}$  observed values,  $\frac{X}{n} = \text{number of determinations}$ 

Coefficient of variation  $=\frac{\epsilon}{X}$ 

Table 2. National Research Corporation

	. Observed values			
•	Sample No. 352	Sample No. 333	Sample No. 354	
	ppm 35.9	270m 106.4	90 pest 21 8 6	
	36.4	108.5	228.3	
	34.4	94. 2	219.8	
	34.6	109. 2	219.2	
	36.3	97. 2	217. 3	
	31.9	108.8	218.2	
	33.6	83.1	221.9	
	31.7	105.3	908.7	
	33.4	\$9.9	224.1	
	32.4	103.2	215. 4	
	34.6	104.0	214.9	
	24.7	89.1	226.7	
	29. D	D8.4	213.5	
		113.8		
Total No. det	18	14	13	
Меал	32.9	100.8	219.0	
Standard dev	3, 1	B.1	5.4	
Coeff. of var%	9.4	8.1	2.5	
Rangeppm	11.2	30.7	19.6 228.8	
High value	35.9 24.7	113.8 83.1	206.7	

	Observed values			
	Bample No. 382	mple No. 352 Sample No. 363		
	ppm 28 34 29 30	⊅рт 86 93 101 97	ppm 214 207 214 210 218	
Total No. det	5 30. 2 3. 1 7. 7 8 34 28	5 93.8 5.2 5.5 13 101 88	5 212.0 3.4 1.6 8 215 207	

Table 4. Allegheny Ludlum Corporation

	Observed values			
	Rample No. 352	Sample No. 353	Sample No. 364	
	99m 34.4 34.2 34.0 33.7 33.7	104 104 104 103 101	129m 227 236 222 220 220 219	
Total No. det	8 33. 6 0. 6 1. 8 1. 7 34. 4 32. 7	103. 0 1. 7 1. 7 4 105 101	6 322 3 3. 3 1. 6 8 227 219	

Table 5. Watertown Arsenal

	Observed values			
	Remple No. 352	Sample No. 863	Sample No. 35	
	рри; 83. Б 33. 4	meger	ppm	
	3,3,6	100.9	221.2	
'	38.4	98.3	216.7	
	31.5	99.0	214.6	
'	29.7	<b>10</b> 1. 1	213.0	
	80. B	95. 8	216.0	
	31.8	102.2	214.7	
	80.6	101.3	211.7	
	29.8	95.4	221. 2	
	32.2	102. 1	217.7	
	32. ť	99. B	212.0	
	32.2	97. 6	218.9	
	30.4	108. 2	214.0	
	30.9	92.6	211.6	
	35.0	101. 3	215.6	
	1	102. 1	216.9	
otal No. det	14	18	16	
lean nom	31,7	99.7	216.3	
andard de√ppm	1.6	8.4	10	
osfiL of var. %	4.7	3.4	1.5	
angeppin_	5.1	13.6	9.6	
igh valueppm	88,0	108. 2	221.2	
w valueppm	29.7	92.6	211.6	

8ample	No. 352	Sample	No, 353	Sample	No, 364]
Ob- served values	Fre- quency	Ob- served values	Fye- quency	Ob- served values	Fre- quency
ppm 91 28 29 30 31	32776	290m 38 80 90 91 92	1 1 8 11	2014 190 202 203 206 207	1 2 4 8
32 33 34 35	7 8 3	25 25 25 27	14 9 6 10 16	208 209 210 211 212	L 10 16 11 12
		98 99 100 101 102	12 7 3 2 1	213 214 215 216 217	8 30 6
				216 219 221	4 1 2
a	(.0 2.2 7.1 8	9. 14 10	5,0 8,1 9.3 4 2		1.8 4.3 2.0 l
	served values  ppm 57 29 30 31 32 33 34 35	served quency values  ppm 37 3 2 2 2 3 3 6 3 4 3 3 5 3 3 5 3 5 5 3 5 5 5 5 5 5 5 5	Observed values  Ppm 37 3 88 29 29 7 90 30 7 91 31 6 92 32 80 34 3 95 35 3 88 97 98 98 99 100 101 102	Observed quency served quency values    Ppm   37   3   88   1   29   2   80   1   1   1   1   1   1   1   1   1	Observed values

TABLE 7. Sample No. 352

Group III					
Laboratory	Mean	ď	ęr.		
Nat'l Res, Corp. Wutertown Arsenal. Battalle Mem. Inst. Dupont Co. Allegheny Laidlum Corp. Nat'l Bur. Standards.	97m, 32.9 31.7 30.9 30.2 33.8 31.0	Ppm 1. 15 -0. 05 -1. 56 -2. 05 -0, 75	1, 33 0, 72 2, 40 4, 20 0, 56		

Z=190, 5 Average 31, 75

Zd"=9. 20 Standard dev. = 1, 356 Standard error = 0, 554 95% confidence limits = 31.8±1.4 ppm.

Adopted value for Group III 32±2 ppm

NOTE: In tables 7 through 9 the 95 percent confidence limits were computed as follows:

96 percent Confidence limits =  $\overline{X} \pm i \frac{1}{\sqrt{\pi}}$ 

where X=average,

z=atanderd deviation,
n=number of ighoratories,
t=2.071 is the critical value of "f" as
given, for example, by Yooden [3].

Table 8. Sample No. 358						
Group II						
Laboratory	Mean	ď	¢2			
Nat'l Res. Corp	2070 100. 2 99. 7	рут 2.3 1.7	5. 29 2. 99			
Batteile Mem. Inst	98. 4 93. 6 103. 0 95. 0	-1.6 -4.2 5.0 -3.0	2, 56 17, 64 26, 00 9, 00			

2=689, 2 Average 98.0

Zd<sup>2</sup>=02, 38 Standard dev, =3.532

Standard error = 1, 442 96% confidence limits = 96, 0±3, 7 ppm,

Adopted value for Oroup II 98±5 ppm

Table 9. Sample No. 354

Group I					
Laboratory	Mean	ď	ą:		
Nat'l Res. Corp. Watertown Arsenal Battelle Mom. Inst. Dupont Co. Allegbeny Lodinm Corp. Nat'l Bur. Standards	97274 219. 0 215. 4 209. 0 212. 0 222. 3 211. 8	ppm 4.1 0.5 -8.0 -2.0 7.4 -3.1	26. 81 0. 25 34. 81 8. 41 54. 78 9. 61		

Z = 1299. 5 A versue 214. 9

 $3d^3 = 124,66$ 

9 Standard dev. =4,998 Standard error =2,038 96% confidence Units=214,9±3,2 ppm.

Adopted value for Group 1 215±6 ppm

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